### <span id="page-0-0"></span>**LMH6672 Dual, High Output Current, High Speed Op Amp General Description Features**

The LMH6672 is a low cost, dual high speed op amp capable of driving signals to within 1V of the power supply rails. It features the high output drive with low distortion required for the demanding application of a single supply xDSL line driver.

When connected as a differential output driver, the LMH6672 can drive a 50 $\Omega$  load to 16.8 V<sub>PP</sub> swing with only −98 dBc distortion, fully supporting the peak upstream power levels for upstream full-rate ADSL. The LMH6672 is fully specified for operation with 5V and 12V supplies. Ideal for PCI modem cards and xDSL modems.

### **Applications**

- ADSL PCI modem cards
- xDSL external modems
- $\blacksquare$  Line drivers
- $\blacksquare$  **High Output Drive** 19.2 V<sub>PP</sub> differential output voltage, R<sub>L</sub> =  $50\Omega$ 9.6 V<sub>PP</sub> single-ended output voltage, R<sub>L</sub> = 25 $\Omega$
- High Output Current
- $\pm 200$  mA @  $V_{\text{O}} = 9$   $V_{\text{PP}}$ ,  $V_{\text{S}} = 12V$ ■ Low Distortion 105 dB SFDR @ 100 kHz,  $V_{O} = 8.4 V_{PP}$ , R<sub>L</sub> = 25Ω
- 98 dB SFDR @ 1MHz,  $V_{\text{O}} = 2 V_{\text{PP}}$ , R<sub>L</sub> = 100 $\Omega$
- High Speed
	- 90 MHz 3 dB bandwidth  $(G = 2)$ 135 V/µs slew rate
- **n** Low Noise
	- 3.1 nV/ $\sqrt{Hz}$  : input noise voltage 1.8 pA/ $\sqrt{Hz}$  : input noise current
- Low supply current: 7.2mA/amp
- Single-supply operation: 5V to 12V
- Available in 8-pin SOIC and PSOP

### **Connection Diagram**



# **Typical Application**



**Figure 1**

**FIGURE 1.**

### **Ordering Information**



April 2004

### **Absolute Maximum Ratings [\(Note 1\)](#page-2-0)**

**If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/ Distributors for availability and specifications.**





# **Operating Ratings** [\(Note 1\)](#page-2-0)



### **Electrical Characteristics**

 $T_J = 25^{\circ}$ C, G = +2, V<sub>S</sub> = ±2.5 to ±6V, R<sub>F</sub> = R<sub>IN</sub> = 470 $\Omega$ , R<sub>L</sub> = 100 $\Omega$ ; Unless otherwise specified.



### <span id="page-2-0"></span>**Electrical Characteristics** (Continued)



**Note 1:** Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but specific performance is not guaranteed. For guaranteed specifications and the test conditions, see the Electrical Characteristics. **Note 2:** Human body model, 1.5kΩ in series with 100pF. Machine model, 200Ω in series with 100pF.

Note 3: Shorting the output to either supply or ground will exceed the absolute maximum T<sub>J</sub> and can result in failure.

**Note 4:** The maximum power dissipation is a function of T<sub>J(MAX)</sub>, θ<sub>JA</sub> and T<sub>A</sub>. The maximum allowable power dissipation at any ambient temperature is P<sub>D</sub> =  $(T_{J(MAX)} - T_A)/\theta_{JA}$ . All numbers apply for packages soldered directly onto a PC board.

**Note 5:** Typical values represent the most likely parametric norm.

**Note 6:** All limits are guaranteed by testing, characterization or statistical analysis.

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#### **Typical Performance Characteristics** (Continued)  $V_{OS}$  vs.  $V_S$  **v**s.  $V_{CM}$ ,  $V_S$  = 12V  $\mathbf{3}$  $\mathbf{1}$  $\mathbf 2$  $0.5$  $\mathbf{1}$  $-40^{\circ}$ C  $25^{\circ}$ C  $V_{OS}$  (mV)  $V_{OS}(mv)$  $-40^{\circ}$ C  $25^{\circ}$ C  $\downarrow$  $\overline{\phantom{a}}$  $\overline{0}$ ╫  $\mathbf 0$  $\vert \hspace{0.1cm} \pmb{\uparrow} \vert$ 85°C  $-1$ 1  $-0.5$ 85°C  $-2$  $-1$  $-3$ 5 6 7 8 9 10 11 12 13 14 15 -0.5 1 2.5 4 5.5 7 8.5 10 11.5 13  $3 \quad 4$  $\mathrm{V_{S}}\left( \mathrm{V}\right)$  $V^{\text{CM}}(V)$ 20016629 20016631  $V_{OS}$  vs.  $V_{CM}$ ,  $V_S = 5V$  Bias Current vs.  $V_{SUPPLY}$  $\mathsf 3$  $10$  $85^{\circ}$ C  $25^{\circ}$ C  $\mathbf 2$ INPUT BIAS CURRENT (µA)  $\bf 8$  $-40^{\circ}$ C 1  $\overline{1}$  $25^\circ$  $85^{\circ}$ C  $V_{OS}$  (mV)  $\boldsymbol{6}$  $\mathbf 0$  $\overline{\mathbf{4}}$  $-1$  $\mathbf 2$  $-2$  $-3$  $\pmb{0}$  $-0.5$  0 0.5 1 1.5 2 2.5 3 3.5 4 4.5 5  $\overline{\mathbf{c}}$  $\overline{\mathbf{4}}$ 6 8  $10\,$ SUPPLY VOLTAGE (V)  $V_{CM} (V)$ <sup>20016630</sup> <sup>20016636</sup> **Offset Current vs. V<sub>SUPPLY</sub> and SUPPLY V**<sub>OUT</sub> **VS. V<sub>IN</sub>**  $0.1$  $\overline{3}$  $T_J = -40^{\circ}$ C to 85°C  $\overline{2}$  $0.08$  $\mathbf{1}$  $-40^{\circ}$ C oFFSET (IA)  $V_{\text{IN}}$  (mV)  $25^{\circ}$ C  $0.06$  $\pmb{0}$  $\bar{t}$ ...<br>85°C  $-1$  $0.04$  $-2$  $R_L = 1k\Omega$  $0.02$  $-3$  $\mathbf 2$  $\bf 6$ 8  $10$  $12$  $14$  $\overline{\mathbf{4}}$  $-2.5$   $-2$   $-1.5$   $-1$   $-0.5$  0 0.5 1 1.5 2 2.5  $V_{\text{SUPPLY}}(V)$  $V_{OUT} (V)$ 20016637 20016639

-40°C

 $12$ 

 $14$ 



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## **Typical Performance Characteristics** (Continued)

### **Harmonic Distortion vs. Output Voltage Harmonic Distortion vs. Output Voltage**

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┭ 3RD

8 9 10 11

4 5 6 7

 $-115$ 

 $-125$ 

 $\mathbf 0$  $\overline{1}$ 



#### **Harmonic Distortion vs. Frequency Harmonic Distortion vs. Frequency**





20016650

100

 $6.8\,$  $6.7$ 

 $6.6\,$ 

6.5

 $6.4$ 

 $6.3$ 

6.2

 $6.1$ 

 $6\phantom{a}$ 

 $5.9\,$ 

5.8

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 $e_n$  &  $i_n$  vs. Frequency,  $V_s = 5V$  and 12V 100 00 /OLTAGE NOISE (nV/Hz) CURRENT NOISE (pAVHZ  $10$ 100  $1<sub>k</sub>$  $10k$ 100k  $1M$ 10M FREQUENCY (Hz)

#### 20016610

### **Application Notes**

#### **THERMAL MANAGEMENT**

The LMH6672 is a high-speed, high power, dual operational amplifier with a very high slew rate and very low distortion. For ease of use, it uses conventional voltage feedback. These characteristics make the LMH6672 ideal for applications where driving low impedances of 25-100Ω such as xDSL and active filters.

A class AB output stage allows the LMH6672 to deliver high currents to low impedance loads with low distortion while consuming low quiescent supply current. For most op-amps, class AB topology means that internal power dissipation is rarely an issue, even with the trend to smaller surface mount packages. However, the LMH6672 has been designed for applications where high levels of power dissipation may be encountered.

Several factors contribute to power dissipation and consequently higher junction temperatures. These factors need to be well understood if the LMH6672 is to perform to specifications in all applications. This section will examine the typical application that is shown on the front page of this data sheet as an example. (*[Figure 1](#page-0-0)*) Because both amplifiers are in a single package, the calculations will for the total power dissipated by both amplifiers.

There are two separate contributors to the internal power dissipation:

- 1. The product of the supply voltage and the quiescent current when no signal is being delivered to the external load.
- 2. The additional power dissipated while delivering power to the external load.

The first of these components appears easy to calculate simply by inspecting the data sheet. The typical quiescent supply current for this part is 7.2 mA per amplifier, therefore, with  $a \pm 6$  volt supply, the total power dissipation is:

 $P_D = V_S$  x 2 x  $I_Q = 12$  x (14.4x10<sup>-3</sup>) = 173 mW  $(V<sub>S</sub> = V<sub>CC</sub> + V<sub>EE</sub>)$ 

With a thermal resistance of 172˚C/W for the SOIC package, this level of internal power dissipation will result in a junction temperature  $(T<sub>J</sub>)$  of 30°C above ambient.

Using the worst-case maximum supply current of 18 mA and an ambient of 85˚C, a similar calculation results in a power dissipation of 216 mW, or a  $T_J$  of 122 $^{\circ}$ C.

This is approaching the maximum allowed  $T_J$  of 150°C before a signal is applied. Fortunately, in normal operation, this term is reduced, for reasons that will soon be explained.

The second contributor to high  $T<sub>J</sub>$  is the power dissipated internally when power is delivered to the external load. This cause of temperature rise is more difficult to calculate, even when the actual operating conditions are known.

To maintain low distortion, in a Class AB output stage, an idle current,  $I_{\Omega}$ , is maintained through the output transistors when there is little or no output signal. In the LMH6672, about 4.8 mA of the total quiescent supply current of 14.4 mA flows through the output stages.

Under normal large signal conditions, as the output voltage swings positive, one transistor of the output pair will conduct the load current, while the other transistor shuts off, and dissipates no power. During the negative signal swing this situation is reversed, with the lower transistor sinking the load current while the upper transistor is cut off. The current in each transistor will approximate a half wave rectified version of the total load current.

Because the output stage idle current is now routed into the load, 4.8 mA can be subtracted from the quiescent supply current when calculating the quiescent power when the output is driving a load.

The power dissipation caused by driving a load in a DSL application, using a 1:2 turns ratio transformer driving 20 mW into the subscriber line and 20 mW into the back termination resistors, can be calculated as follows:

 $P_{DRIVER} = P_{TOT} - (P_{TERM} + P_{LINE})$  where

 $P<sub>DRIVEB</sub>$  is the LMH6672 power dissipation

 $P_{TOT}$  is the total power drawn from the power supply

 $P<sub>TERM</sub>$  is the power dissipated in the back termination resistors

 $P_{LINE}$  is the power sent into the subscriber line

At full specified power,  $P_{\text{TERM}} = P_{\text{LINE}} = 20 \text{ mW}$ ,  $P_{\text{TOT}} = V_{\text{S}}$  $x \mid_{S}$ .

In this application,  $V_S = 12V$ .

 $I_S = I_Q + A_{VG} I_{OUT}$ 

 $I_{\Omega}$  = the LMH6672 quiescent current minus the output stage idle current.

### **Application Notes** (Continued)

#### $I<sub>Q</sub> = 14.4 - 4.8 = 9.6$  mA

 $\mathsf{A}_{\mathsf{VG}}$  II<sub>OUT</sub>I for a full-rate AD<u>SL CPE a</u>pplication, using a 1:2 turns ratio transformer, is  $\sqrt{(40 \text{ mW}/50 \Omega)} = 28.28 \text{ mA RMS}.$ 

For a Gaussian signal, which the DMT ADSL signal approximates, A<sub>VG</sub> II<sub>OUT</sub>I =  $\sqrt{2/\pi}$  x I<sub>RMS</sub> = 22.6 mA. Therefore, P<sub>TOT</sub> = (22.6 mA + 9.6 mA) x 12V = 386 mW and P $_{\rm DRIVER}$  is 40 = 346 mW.

In the SOIC package, with a  $\theta_{JA}$  of 172°C/W, this causes a temperature rise of 60˚C. With an ambient temperature at the maximum recommended  $85^{\circ}$ C, the T<sub>J</sub> is at 145 $^{\circ}$ C, well below the specified 150˚C maximum.

Even if we assume the absolute maximum  $I_S$  over temperature of 18 mA, when we scale up the  $I<sub>O</sub>$  proportionally to 7 mA, the  $P_{DRIVER}$  only goes up by 41 mW causing a 62°C rise to 147˚C.

Although very few CPE applications will ever operate in an environment as hot as  $85^{\circ}$ C, if a lower  $T_{J}$  is desired or the LMH6672 is to be used in an application where the power dissipation is higher, the PSOP package provides a much lower  $\theta_{JA}$  of only 58.6°C/W.

Using the same  $P_{DRIVER}$  as above, we find that the temperature rise is only 19° and 21°C, resulting in  $T_j$ 's in an 85°C ambient of 104˚C and 106˚C respectively.

#### **CIRCUIT LAYOUT CONSIDERATIONS**

National Semiconductor suggests the following evaluation boards as a guide for high frequency layout and as an aid in device testing and characterization. Since the exposed PAD (or DAP) of the PSOP package is internally floating, the footprint for DAP could be connected to ground plane in PCB for better heat dissipation.



These free evaluation boards are shipped when a device sample request is placed with National Semiconductor.



**LMH6672**

### **Notes**

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